**Investigation of the Performance of Model Predictive Control for Induction Motor Drives**

**Ahmed G. Mahmoud A. Aziz1, Hamdi Ali2, Yehia Sayed Mohammed3, Ahmed A. Zaki Diab4\***

1,3,4Dep. of Electrical Engineering, Faculty of Engineering, Mina University, Minia, Egypt.

1,2Dep. of Electrical and Computer Engineering, El\_Minia High Institute of Engineering and Technology, Minia, Egypt.

Abstact: The current work presents speed, torque and flux control of an induction motor (IM) drive, founded on model predictive control (MPC). Via the MPC techniques, the motor electromagnetic torque and flux linkage are controlled as an internal loop. However, the speed is controlled as the external loop. The internal control loop is founded on finite control set FCS-MPC, and the external control founded on the torque PI controller. The performance of the MPC is tested with various conditions of the drive operation, and the outcomes approve the excellent steady-state and dynamic operation of the system in a wide range of speeds and with torque disturbance.

Keywords: Induction Motor; Model Predictive Control; Finite Control Set

# **Introduction**

The Direct Torque Control (DTC) method selects the calculated magnitude of stator ﬂux and the calculated torque as the two control state variables. It utilizes a closed-loop feedback control assembly to make the flux and torque errors not exceed the hysteresis band (a predetermined band limit) [1-4]. The errors are estimated as the variance between the reference and the calculated value of the flux and torque. DTC requires the application of hysteresis band comparators as an alternative of flux and torque controllers. The DTC employs a pre-deﬁned search table to choose the switching procedure based on the inverter mode. Merits of DTC strategy are concise as, rapid transient response, easy configuration and minimal parameter reliance [3-6]. However, the old DTC method has the disadvantages of significant-high torque and ﬂux spikes. As probable substitute control plans, model prognostic control. The DTC is assuring the straight selection of the suitable switch states.

MPC employed to power electronics has two chief variations: Continuous Control Set MPC (CCS-MPC) [5], [6] and FCS-MPC [6]. The CCS-MPC estimations use the result of an adjusted drawback and a modulation phase produces a switch state of the converter stimulation. FCS-MPC utilizes the separate character of the power converter and a model of the load to resolve the adjustment problem comprehensively. FCS-MPC was utilized in many purposes, like conventional 3-phase 2-level converters [8], [9].

Lately, MPC has gotten a high consideration in power electronics and motor drives because of the compensations of simple perception, fast-answer in addition to an excessive ﬂexibility to include numerous restraints [10–12]. Several investigations have been performed on the correlated application of the MPC in power electronics and drives. Limited Control Set MPC (FCS-MPC), between MPC methods, is the exclusive one because of the discrete character of an inverter and giving the best solution for the on-line optimization challenge. Additionally, easy digital employment and guarantee of non-linearities and restraints of MPC were additional characteristics of this algorithm [13-15].

 The Predictive Torque Control (PTC) method, utilizing FS-MPC in directly torque&flux controlling of an induction machine, was introduced in [16]. In PTC for an induction machine, a rule like the DTC is employed [1]. The core attention of PTC is the estimate of the torque and stator flux for every probable inverter switching modes. At that time a pre-defined cost-function estimates forecast values and lastly, a trajectory that has a minimum cost-function is elected. The system constrictions, numerous control objects and variables may be added to the cost-function simply. This plan doesn’t want Park transformation, exterior tuner, tuning technique of the controller’s components and internal current control loop. However, PTC wants a sampling of high frequency to achieve the best performance. The Implementation of PTC algorithm extends the period significantly, and this leads to the sampling of low -frequency and unsought influences on the functioning of the drive system.

Wang, Demonstrated the FS–MPC as a modern method. FS–MPC is more straight forward in the concept of design, it has a fast dynamic and good torque response; the experimental results verify that all strategies theoretical [17].

Shafiq Odhano, Stated that an MPC as a substitute to the linear controller-based Direct flux and current vector control of induction machines, a judgment among MPC and PI controller, was performed by experimentation. Simultaneously, the FCS-MPC outcomes in stator current with rich harmonic content that negatively affects the drive presentation and efficiency. However, MPC has benefits over PI regulator in that the controller tuning is not essential with MPC [18].

Cristian Garcia, presented a cascaded construction for the control of an induction-machine which is concerned utilizing the FCS-MPC. The strategy of control has two loops, external and internal. The external loop control is for the speed. In contrast, the internal loop controls the current of the stator. The experimental consequences illustrate that the planned strategy has a performance that is matching the classical control plans but that it is overshoot-free and gives an improved response time [19].

# **MATHEMATICAL MODEL of THE IM**

In the current reference framework, the stator voltage of IM consists of a stator resistance voltage decrease and the alteration rate of the stator flux linkage. The stator voltage function of the motor in the stationary reference setting (α-β) may be described as follows [1]:

 (1)

Where,

 , and

The electromagnetic torque equation has the following expression: ) (2)

The dynamic mechanical system equation may be presented in the subsequent method:

 (3)

The rotor angular speed is given as the time differentiation of the rotor position angle:

  (4)

Preserving the stator flux to be constant, the difference of the electromagnetic torque (Te) depending on the path of the used voltage vector, such that:

 (5)

where  is the angular speed of the stator flux linkage relative to rotor flux linkage. The equation of torque demonstrates that the torque could be controlled via controlling the relative speed among the stator and rotor flux at steady stator flux amplitude. As the electrical time constant is significantly lower than the mechanical time constant, the torque could be controlled via controlling the velocity of stator flux.

# **The dynamic model of the IM**

The dynamic model of the induction motor at rest can be mentioned by the differential equations [25]:

 (6)

 (7)

 (8)

 (9)

 (10)

where:

|  |  |
| --- | --- |
|  Magnetic inductance (H)  Rotor self-leak inductance (H)M Mutual inductance (H) Stator self-leak inductance (H) Leak coefficient  Load torque and Electromagnetic torque (Nm) Stator resistance and Rotor resistance (Ω) Synchronous velocity (rad/sec) Command slip velocity (rad/sec) Actual and Reference Rotor velocity (rad/sec) Angle among the synchronous and stationary frames  |  Rotor time constant  The Load damp coefficient  Inertia Moment (kg.), rest axes stator current values (A) , Synchronous axes stator current values (A) Synchronous axes desired stator currents values Rotor flux vector (wb) , Stationary axes rotor flux values (wb)  , Synchronous axes rotor flux values (wb) Differential operator () poles number |

# **Derect Torque Control of IM**

The selection of the stator voltage vector regarding the difference among the reference flux & torque and their real values is the basic principle of DTC [1-6]. To generate digital signals, the errors are fed over the separate hysteresis band matchers. A 3D look-up table subsequently choose the suitable voltage vector to fulfill the flux & torque commands. The compensations of DTC strategy are briefed as a simple configuration, fast transient reply, and fewer parameter requirements [3-6].

The DTC is guaranteeing the straight selection of the optimal switch-modes, and so the stator voltage vector so as to retain the flux& torque errors does not exceed the hysteresis band (a predetermined band limit) [1-3]. The errors were estimated by the variance among the reference and the estimated values of the flux &torque dissimilar to the field-oriented control. DTC needs the use of hysteresis band comparators in place of flux & torque controllers. The DTC utilizes a look-up table to choose the switching process founded on the states of the inverter. The stator flux linkage components can be getting it from the following equations:

 (11)

 (12)

Where and were the primary condition of the stator flux parameters. For the induction motor, the primary values of the stator flux were set to zero [1].

 The value of the stator flux could be calculated as:

 (13)

The electromagnetic torque could be calculated by the stator current and the calculated stator flux as:

 (14)

If the time period is appropriately short, ignoring the voltage drop of stator resistance, the practical voltage space vector gives a stator flux alteration having a similar path of the voltage space vector. The value of the stator flux space vector was reserved stable by the application of the suitable voltage space vectors. Simultaneously, the phase angle of the stator flux space vector may be quickly altered by the application of voltage space vectors, resulting a fast alteration of the torque angle. Then the electromagnetic torque could be quickly altered by altering the torque angle in the needed path.

Briefly, the torque may be controlled by voltage space vectors. For every part, two voltage vectors were chosen to raise or reduce the value of stator flux. A look-up table gives the switching states to the control of hight and direction of the stator flux. In this table, θS is the area number for the stator flux linkage, Hψ is the outputs of the hysteresis controllers for flux linkage and HT is for torque. The block drawing of an IM drive with velocity control founded on DTC scheme is presented in Fig. 1. The stator currents& voltages are measured and converted into equivalent α-β values. The stator flux and electromagnetic torque are assessed by measuring the current& voltage. Alternatively, the motor velocity is matched with the reference one to produce the torque command. The torque& flux commands are matched with the equivalent calculated values and the errors are fed within the respective hysteresis band comparators so as to produce a digital signal. A 3D look-up table at that time picks out the suitable voltage vector to fulfill the flux & torque commands. The controlling switching states of the amplitude & direction of the stator flux are shown in a look-up table [5].

Figure 1. DTC scheme

1. **Proposed MPC based IM drive**

## Basics of Model Predictive Control (MPC)

Model predictive control is one of the best methods of control because of its merits of rapid dynamic reply, intuitive concept, the capability to handle many nonlinear limitations multivariable control, and so on. For induction motors of high-performance frequently torque and stator flux are elected like a control variable. In conventional MPC, a cost-function concerning the torque & flux errors is outlined and assessed for every voltage vector and the one minimalizing the cost-function is elected like the best voltage vector [14].

The MPC where the system model is taken into account so as to count the upcoming performance of the variables within a time frame (integer multiplication of the sample period). These estimates are founded on a cost-function and subsequently reduces the cost-function is selected, finding, in this method, the upcoming control activities. Solitary the ﬁrst value of the order is used, and the algorithm is considered each sample time again. MPC has numerous compensations as the simple presence of nonlinearities and restrictions. This arrangement has limited uses in the power converter control and drives because of the high values of calculations required so as to resolve the regulation drawback online [24].

An additional method for implementing MPC in the power converters and drives was to utilize the benefit of the power converters discontinuous character. Although the power converters have limited switching states, the MPC optimization difficulty could be simpliﬁed and decreased to the estimate of the system performance solitary for those probable switching states. So, every estimate is employed to assess a cost-function (also identified as quality or decision function) and subsequently, the state with the smallest cost is elected and created. This method is identified as a FCS-MPC; also the probable control deeds (switching states) are limited. This technique additionally identified as limited alphabet MPC or easily as predictive control, and it was effectively functional to a widespread-range of the power converter and drive uses [21].

Figure 2. General MPC Scheme

## Model predictive control (MPC) scheme

MPC is one of the most best control approaches because of its qualities of obvious concept, multi-variable control, rapid dynamic response, capability to handle several nonlinear constraints, a model of the arrangement is measured so as to expect the upcoming performance of the variable quantity over a time frame, These calculations are assessed founded on a cost-function, and then, the arrangement that reduces the cost-function is selected, gaining, in this method, the upcoming control actions. Only the ﬁrst value of the order is used, and the algorithm is intended once more every sampling period.

A block drawing of the predictive control arrangement is introduced in Fig. 2. Quantities of several variables x(k), as currents, voltages and velocity, were employed by the predictive model to compute the upcoming values of the controlled variables x(k +1) for the complete probable voltage vectors. These calculations are assessed via the cost-function regarding the reference values x∗(K). The voltage vector (or switching state) that reduces the cost-function is elected and used within the following sampling time. The subsequent paragraphs give several examples of the applications of the control scheme. Altogether the control arrangements were estimated via a cost-function g and a discrete-period model employed in calculation. It is revealed that the error of the load current, the torque&ﬂux in an induction machine, the rapid power and the DC connection voltage are variables that could be controlled.

## Predictive torque control (PTC) method

The PTC, utilizes the basis like to DTC. In this arrangement, the best voltage vector is elected by approximation, calculation and cost-function optimizing technique [22]. An easy prognostic torque control arrangement is introduced in Fig. 3. In PTC technique, the stator&rotor flux at the current sampling stage k are assessed. The stator&rotor flux estimate can be calculated by:

 (15)

 (16)

Where is the assessed value of and is sampling period.

# **Torque and Flux Prediction**

A Guess of the stator flux and electromagnetic torque T for every voltage vectors of 2L-VSI necessary to be performed. The stator flux will be guessed:

 (17)

The torque calculation is connected to the calculated stator flux and current values; thus, the torque calculation function is:

 (18)

It is essential to guess the stator current for instant k+1. In this circumstance, the current calculation is,
 (19)

The stator flux was introduced in relations of the inverter voltages , thus 7-various calculated stator flux and torque values are gotten. The values are assessed in a cost-function is chosen as the best vector. In the conventional PTC Arrangement, the subsequent cost-function is employed : (20)

where is the weighting factor that introduce the control objects rank.

# **Control Scheme based MPC**

Recently, a lot of studies were performed on the MPC implementation in the drives and power electronics. The MPC methods that have been employed in Power Electronics were categorized into two core types [12], [14]: FCS-MPC and Continuous Control Set MPC. In the ﬁrst set, a modulator produces the switching states beginning from the predictive controller continuous output. On the contrary, the FCS-MPC method uses the benefit of the switching states fixed number of the power converter for resolving the regulation limitation. A disconnected model was employed to expect the performance of the system for each allowable actuation arrangement up to the prediction limit. The switching act that reduces a pre-deﬁned cost-function is eventually designated to be used in the next sampling period. The chief benefit of FCS-MPC was the straight use of the control action to the converter, with no need of a modulation stage [23-24].

PTC for an induction machine, a basis like the DTC was employed. PTC method, using FS-MPC in direct torque & flux control of induction machine, the basis of PTC is the estimate of the torque and stator flux for every possible inverter switching states. A pre-defined cost-function assesses predicted values, and eventually, a vector by lessening the cost-function is elected. The system restrictions, some control items and variables can be easily added to the cost-function. This plan doesn’t require Park transformation, external modulator, modification practice of the controller’s parameters and the loop of internal current control [5].

Expensive DSP or FPGA hardware must be introduced to surmount the high computational problem of this algorithm. Furthermore, the limited amount of the inverter switching states, laterally with the opportunity of using numerous successive switching states, leading to adjustable switching frequency. These 2 core disadvantages lead to difficulties of the implementation of PTC in industrial systems [7].

Concerning the complex computational problem, it was proved that the number of permissible switching states of an inverter has a high effect. So, multi-level converter approaches are not extensively utilized with FS-PTC in industrial uses [9], [10].



Figure 3. PTC scheme

# **Results**

Parameters of the IM drive are listed in appendix. The IM drive based MPC has been tested under operation conditions using the proposed control scheme of figure 3. The measured values and the reference electrical torque, the reference and actual speed, the stator currents, and the stator flux are given in different cases in order to demonstrate the drive performance.

## Case 1

Figure 4 displays the act of the drive system at forward and opposite velocity, the amplitude of stator flux with a stable value of 0.71 wb. And the timing sequence as following, At t = 0 the motor is started, during 2 sec reference speed is increased linearly up to 10 rps, and kept constant for two second, at t = 4 sec reference speed decreases linearly up to -10 rps and kept constant for two seconds, at t = 8 sec the reference speed goes to zero rps in two seconds, the load torque is kept constant at 10 N.m during simulation period, from the consequences, a good dynamic act has been accomplished at the circumstance of changing speed in forward and reverse, and it may be noticed that the real electrical torque could follow the reference torque splendidly.



Figure 4. The performance of IM drive-based MPC for Case 1

## Case2

 Figure 5 shows the real velocity can track the reference velocity, the phase current is sinusoidal, and the amplitude of stator flux with a stable value of 0.71 wb. While the timing sequence as following, At t = 0 the motor is started, during 2 sec reference speed is increased linearly up to 10 rps, and kept constant for two second, at t = 4 sec reference speed decreases linearly up to -10 rps and kept constant for two second, at t = 8 sec the reference speed goes to zero rps in two second, the torque of the load is

reserved steady at 18 N.m during simulation period, from the consequences, an excellent dynamic act was accomplished at the circumstance of altering velocity in forward and opposite, and it could be noticed that the real electrical torque can follow the reference torque wonderfully.



Figure. 5. The performance of IM drive based MPC for Case 2

Case3
 Figure 6 displays the act of the drive system at forward and opposite velocity, stator flux height with stable level of 0.71 wb. At t = 0 the motor is started, during 2 sec, reference speed is increased linearly up to 200 rps, and kept constant for two second, at t = 4 sec reference speed decreases linearly up to -200 rps and

kept constant for two second, at t = 8 sec the reference speed goes to zero rps in two second, the load torque is reserved steady at 10 N.m within simulation period, from the consequences, a better dynamic act has been accomplished at the circumstance of changing speed in forward and reverse.



Figure 6. The performance of IM drive based MPC for Case 3

Case4
 The consequences demonstrate the real velocity can track the reference speed, and the stator flux height with constant amount of 0.71 wb. And the timing sequence as following, At t = 0 the motor is started, during 2 sec reference speed is increased linearly up to 200 rps, and kept constant for two second, at t = 4 sec reference speed decreases linearly up to -200 rps and kept constant for two second, at t = 8 sec the reference speed goes to zero rps in two second, the load torque is kept constant at 13 N.m during simulation period. The performance of such case of study has been shown in figure 7.



Figure 7. The performance of IM drive based MPC for Case 4

Case5 The results evidenced a good dynamic performance, quick recovering from load disturbance, the phase current is sinusoidal, And the timing sequence as following, A 5 N.m loading torque is employed on the motor at starting, after 2 sec and is changed to 19 N.m and return to 5 N.m at t = 4 sec and it kept at this value

within the residual simulation interval, the reference speed remains constant at 10 rps during simulation period, the results show the over-shoot and dip of the actual velocity. The performance of MPC based drive has been shown in figure 8.



Fig. 8. The performance of IM drive based MPC for Case 5

# **CONCLUSIONS**

A model predictive controlling of induction motor drives is ‎introduced in the current work. The FS-MPC is a modern method for ‎electrical drive systems which has fast dynamics and good torque ‎response. The controller controlled straight the inverter ‎switches to follow the velocity path of the IM, the ‎controller does well in following the velocity path at low ‎and high velocity. A cost-function involving of following error ‎of stator flux and electromagnetic torque to elect the finest ‎voltage vector, the MPC controller has several compensations. In addition of being simple to construct and to be implemented, it has ‎a very rapid reply, lesser ripples over currents and ‎electromagnetic torque relative to the traditional ‎DTC approach. The simulation consequences display ‎that the drive reply has several benefits: very rapid ‎reply, robustness in contradiction of load variations and well following-up ‎of velocity path at both low & high speeds.

# **REFERENCES**

‎[1]‎ I. Takahashi and T. Noguchi, “A new quick-response and high-‎efﬁciency control strategy of an induction motor”, IEEE Trans. ‎Ind. Electron.,vol. IA-22, no. 5, pp. 820–827, Sep. 1986.‎

‎[2]‎ ‎ M. A. Rahman, and M. A. Hoque, “Sensorless direct torque ‎control of induction motors used in electric vehicle”, IEEE ‎Trans. On Energy Conversion, Vol. 18, No. 1, pp. 1-9, March ‎‎2003.‎

‎[3]‎ Murat Barut, Seta Bogosyan and Metin Gokasan. “Speed ‎sensorless direct torque control of IMs with rotor resistance ‎estimation.”, Energy conversion and management, Vol. 46, pp. ‎‎335-349, 2005.

[4] Sultan H.M., Kuznetsov O.N., Diab A.A.Z., Site selection of large-scale grid-connected solar PV system in Egypt, (2018) Proceedings of the 2018 IEEE Conference of Russian Young Researchers in Electrical and Electronic Engineering, ElConRus 2018, 2018-January , pp. 813-818.

‎[5]‎ Linder, Arne, Rahul Kanchan, Peter Stolze, and Ralph Kennel. "Model-based predictive control of electric drives.", Cuvillier, 2010.

‎[6]‎ Mariethoz, Sebastien, Alexander Domahidi, and Manfred Morari. "High-bandwidth explicit model predictive control of electrical drives.", IEEE Transactions on Industry Applications 48, no. 6 (2012): 1980-1992.

‎[7]‎ Ahmed A. Zaki Diab, Denis A. Kotin. and Vladimir V. Pankratov. "Speed control of sensorless induction motor drive based on model predictive control." In 2013 14th International Conference of Young Specialists on Micro/Nanotechnologies and Electron Devices, pp. 269-274. IEEE, 2013.

‎[8]‎ Mossa, Mahmoud A., Hamdi Echeikh, Ahmed A. Zaki Diab and Nguyen Vu Quynh. "Effective Direct Power Control for a Sensor-Less Doubly Fed Induction Generator with a Losses Minimization Criterion." ,Electronics 9, no. 8 (2020): 1269.

[9] Mohamed I.S., Rovetta S., Do T.D., Dragicevic T., Diab A.A.Z., A neural-network-based model predictive control of three-phase inverter with an output LC Filter, (2019) IEEE Access, 7 , art. no. 8819887 , pp. 124737-124749.

[10] Y. Zhang and C. Qu. "Model predictive direct power control of ‎PWM rectiﬁers under unbalanced network conditions.” IEEE Trans. ‎Ind. Electron., vol. 62, no. 7, pp. 4011–4022, 2015.‎

‎[11]‎ S. Vazquez, J. I. Leon, L. G. Franquelo, J. Rodriguez, H. A. ‎Young,‎ A. Marquez, and P. Zanchetta, “Model predictive control: A ‎review of its applications in power electronics.”, IEEE Ind. Electron. Mag., ‎vol. 8, no. 1, pp. 16–31, March 2014.‎

[12]‎ Y. Zhang, Y. Peng, and H. Yang, “Performance improvement of ‎two vectors-based model predictive control of PWM rectiﬁer.”, ‎IEEE Trans.‎ Power Electron., vol. 31, no. 8, pp. 6016–6030, 2016.‎

‎[13]‎ P. Cortes, M. P. Kazmierkowski, R. M. Kennel, D. E. Quevedo, ‎and J.‎ Rodriguez, “Predictive control in power electronics and drives.”, ‎IEEE Trans. Ind. Electron., vol. 55, DOI 10.1109/TIE.2008.2007480, ‎no. 12,‎ pp. 4312–4324, Dec. 2008.

 ‎‎[14]‎ S. Kouro, P. Cortes, R. Vargas, U. Ammann, and J. Rodriguez, ‎‎“Model‎ predictive control-a simple and powerful method to control ‎power converters.”, IEEE Trans. Ind. Electron., vol. 56, DOI ‎10.1109/IPEMC.2009.5289335, no. 6, pp. 1826–1838, Jun. ‎‎2009.‎

‎[15]‎ J. Rodriguez, M. P. Kazmierkowski, J. R. Espinoza, P. ‎Zanchetta, H. Abu-Rub, H. A. Young, and C. A. Rojas, “State of the art of ‎finite control set model predictive control in power electronics.”, IEEE ‎Trans.‎on Ind. Informatics, vol. 9, DOI 10.1109/TII.2012.2221469, ‎no. 2, pp.‎ ‎1003–1016, May 2013.‎

‎[16]‎ H. Miranda, P. Cortes, J. I. Yuz, and J. Rodriguez, “Predictive ‎torque control of induction machines based on state-space models.”, ‎IEEE Trans. Ind. Electron., vol. 56, DOI 10.1109/TIE.2009.2014904, ‎no. 6,‎ pp. 1916–1924, 2009.‎

‎[17]‎ Fengxiang Wang, Zhenbin Zhang\*, Xuezhu Mei, José Rodriguez ‎and Ralph Kennel, “ Advanced Control Strategies of Induction ‎Machine: Field Oriented Control, Direct Torque Control and ‎Model Predictive Control .”, Energies 2018.‎

‎[18]‎ Shafiq Odhano, Radu Bojoi, Andrea Formentini, Pericle ‎Zanchetta and Alberto Tenconi, “Direct flux and current vector ‎control for induction motor drives using model predictive ‎control theory.”, IET Electr. Power, Vol. 11 Iss. 8, pp. 1483-‎‎1491, Appl., 2017. ‎

‎[19]‎ Cristian Garcia, Jose Rodriguez, Cesar Silva, Christian Rojas, ‎Pericle Zanchetta, and Haitham Abu-Rub, “Full Predictive ‎Cascaded Speed and Current Control of an Induction Machine ” ‎IEEE TRANSACTIONS ON ENERGY CONVERSION, VOL. ‎‎31, NO. 3, SEPTEMBER 2016.‎

‎[20]‎ Ahmed A. Zaki Diab. "Implementation of a novel full-order observer for speed sensorless vector control of induction motor drives." Electrical Engineering 99, no. 3 (2017): 907-921.‎

‎[21]‎ R. Vargas, U. Ammann, J. Rodriguez, J. Pontt, “Predictive ‎Strategy to Reduce Common-Mode Voltages on Power Converters”, in ‎Power Electronics Specialists Conference, PESC 2008, June 2008.‎

‎[22]‎ J. Rodriguez and P. Cortes, "Predictive Control of Power ‎Converters and Electrical Drives.", John Wiley & Sons, 2012.‎

[23] Ahmed A. Zaki Diab, D. A. Kotin, V. N. Anosov, and V. V. Pankratov. "A comparative study of speed control based on MPC and PI-controller for Indirect Field oriented control of induction motor drive." In 2014 12th International Conference on Actual Problems of Electronics Instrument Engineering (APEIE), pp. 728-732. IEEE, 2014.

[24] Ahmed A. Zaki Diab, V. V. Vdovin, D. A. Kotin, V. N. Anosov, and V. V. Pankratov. "Cascade model predictive vector control of induction motor drive." In 2014 12th International Conference on Actual Problems of Electronics Instrument Engineering (APEIE), pp. 669-674. IEEE, 2014.

[25] A. G. M. A. Aziz, A. A. Z. Diab, and M. A. E. Sattar,"Speed sensorless vector controlled induction motor drive based stator and rotor resistances estimation taking core losses into account," in 2017 Nineteenth International Middle East Power Systems Conference (MEPCON), 2017, pp. 1059-1068.

# **Appendix**

Table 1. Parameters of the IM drive

|  |  |  |
| --- | --- | --- |
| Symbol | Parameters | Values |
|  | Rated voltage |  |
|  | No. pole pairs |  |
|  | Rated frequency |  |
|  | Stator resistance |  |
|  | Rotor resistance |  |
|  | Stator self-inductance |  |
|  | Rotor self-inductance |  |
|  | Magnetizing inductance |  |
|  | Moment of inertia |  |
|  | Nominal stator flux |  |
|  | Nominal torque |  |
|  | Core-resistance |  |
|  | Sampling-time |  |
|   | Proportional gain | 3.016 |
|  | Integrative gain | 0.141 |